Law of similarity and Reynolds number:

Constructional systems of fluid physics can be simulated with smaller models! All dimensions of distance I and time t will be scaled to dimensionen of unity L und T and the velocity expressed as L/T !

$$t = t' \cdot T, \quad u = u' \cdot \frac{L}{T}, \quad p = p'(\frac{L^2}{T^2}) \cdot \rho$$
$$l = l' \cdot L \quad \nabla = \frac{\nabla'}{L}, \quad \text{via } p = \frac{force}{area} = \frac{m \cdot acceleration}{area} = \frac{\rho \cdot L^3 \cdot \frac{L}{T^2}}{L^2}$$

The primed quantities are dimensionless!

Navier-Stokes:

$$\rho(\frac{\partial}{\partial t} + (\vec{u} \cdot \vec{\nabla}))\vec{u} = -grad P + \rho \cdot \vec{g} + \eta \cdot \Delta \vec{u}$$
without $\rho \cdot \vec{g}$

$$(\frac{\partial}{\partial t} + (\vec{u}' \cdot \vec{\nabla}'))\vec{u}' = -\nabla' P' + \frac{1}{\text{Re}} \cdot \Delta' \vec{u}'$$

$$\frac{\rho \cdot L^2}{\eta \cdot T} = \frac{\rho \cdot u \cdot L}{\eta} = \text{Re: Reynolds number}$$

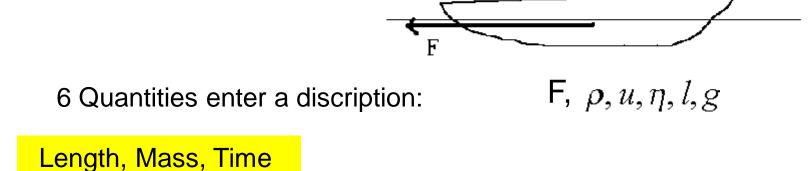
What is the meaning of this number?

$$\frac{\rho \cdot u \cdot L}{\eta} \quad \text{Expansion with } L^2 u: \quad \frac{\rho \cdot u^2 \cdot L^3}{\eta \cdot L^2 \cdot u} = \boxed{\frac{2 \cdot E_{kin}}{W_{friction}}} = \text{Re}$$

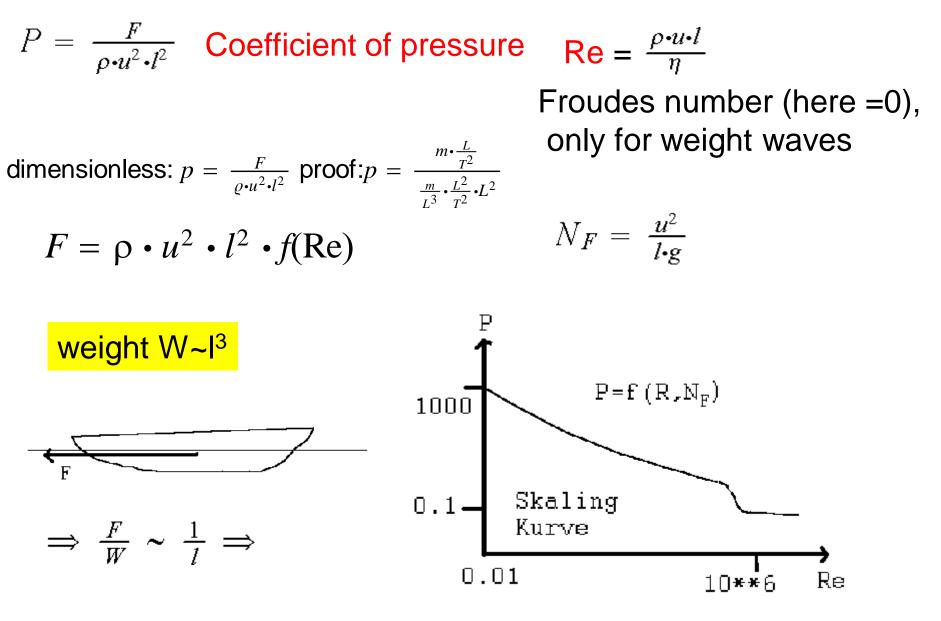
e.g.: from experiment for water pipe: Re=2300

$\gtrsim 2300 \Rightarrow \text{turbulent}$ $\prec 2300 \Rightarrow \text{laminary}$

Other examples, in order to demonstrate the direction of argumentation! Ship in water: Question "Is it more advantageous with respect of fuel economy to build large ships?"



There are 3 relations:



large ships are more cost efficient

Another example: **Rowing**:

What is the difference of speed of an single compared to an eight rower team?

Power of oarsmans: E=F*u~n, n=number of oarsmen

Weight of a team of oarsmen: W~n R=Re

= 0.7937

$$\frac{E}{W} = \frac{\rho \cdot u^3 \cdot l^2 \cdot f(R)}{\rho \cdot l^3} = \frac{u^3 \cdot f(R)}{l}$$
 Does not explicitly depend on n!

Single: 6.33

7.10 5.54

8

7

I, the size of the boat, design for water displacement, depends via $W = \rho \cdot l^3 \sim n$ on n. Men: Min.Sec:

$$\Rightarrow l^{3} \sim n \Rightarrow l \sim \sqrt[3]{n}$$
Because E/W does not depend on n
follows: $u \sim \sqrt[3]{l} \Rightarrow$
 $u \sim \sqrt[3]{\sqrt{n}} = \sqrt[9]{n}$ Men 0.8117
 $\frac{one}{eigth} = \frac{1}{\sqrt{8}} = 0.7937$
Women: 0.82

Women : 0.82

2

0 L

3

4 5

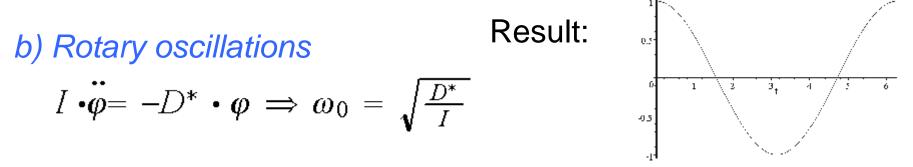
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oarsmen

4. Oscillations and waves *4.1. Free oscillations*



m •*x*: Inertial force $D \cdot x$: Reset force



Damped oscillations:

 $m \cdot x = -k \cdot x - D \cdot x$ or $m \cdot x + k \cdot x + D \cdot x = 0$

 $k \cdot x$ Frictional force

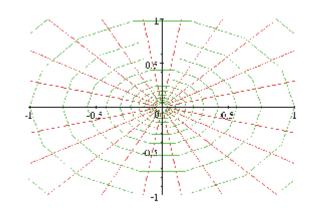
Mathematical structure : Homogene, linear differential equation

Solution with complex numbers: $m \cdot z + k \cdot z + D \cdot z = 0$

Ansatz:
$$z = A \cdot e^{i\gamma t}$$
 γ : complex

Derivation: $\vec{z} = i \cdot \gamma \cdot A \cdot e^{i\gamma t}$

$$\overset{\cdot\cdot}{z=}(i\boldsymbol{\cdot}\gamma)^{2}\boldsymbol{\cdot}A\boldsymbol{\cdot}e^{i\gamma t}=-\gamma^{2}\boldsymbol{\cdot}A\boldsymbol{\cdot}e^{i\gamma t}\Longrightarrow$$



$$-m \cdot \gamma^2 \cdot A \cdot e^{i\gamma t} + i \cdot \gamma \cdot k \cdot A \cdot e^{i\gamma t} + D \cdot A \cdot e^{i\gamma t} = 0$$

hence the characteristic equation: $-m \cdot \gamma^2 + i \cdot \gamma \cdot k + D = 0$

or
$$\gamma^{2} - i \cdot \gamma \cdot k/m - D/m = 0$$

 $\gamma = \frac{1}{2m} \left(ik \pm \sqrt{(-k^{2} + 4mD)} \right) = \delta \cdot i \pm \omega \Rightarrow$
 $z = A \cdot e^{i \cdot (\delta \cdot i \pm \omega)t} = A \cdot e^{-\delta \cdot t} e^{i \cdot \pm \omega t}$
with δ
as damping constant!

$$z = A \cdot e^{i \cdot (\delta \cdot i \pm \omega)t} = A \cdot e^{-\delta \cdot t} e^{i \cdot \pm \omega t}$$

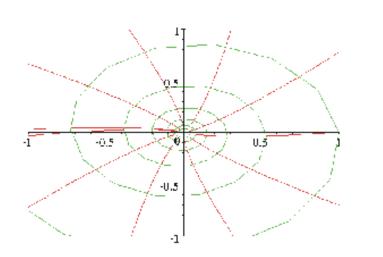
Projection on real part:

$$x = x_0 \cdot e^{-\delta \cdot t} \cdot \cos \omega t$$

0.5

0

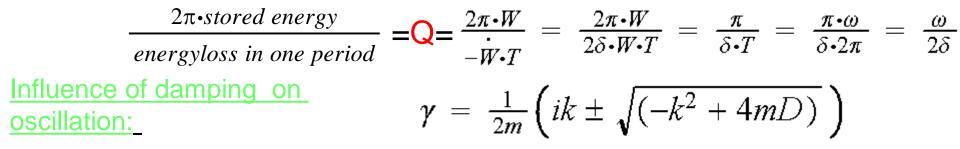
-0.5



Without damping W = $W_{kin} + W_{pot} = \frac{1}{2}m\dot{x}^2 + \frac{1}{2}D \cdot x^2$ Energy of damped oscillator: \dagger_1 T \dagger_2 Oscillates and drops uniformly

From $W = \frac{1}{2}D \cdot x_1^2$ at $x_1(t_- = 0)$ $W = \frac{1}{2}D \cdot x_2^2$ at $x_2(t_- = T)$ $x_2 = x_0 \cdot e^{-\delta \cdot T} \cdot \cos \omega T \Rightarrow W = \frac{1}{2}D \cdot x_0^2 e^{-2\delta \cdot t}$

Definition of figure of merit of a set-up:



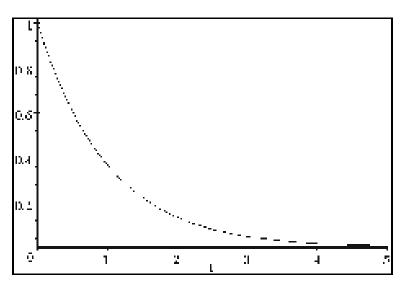
3 cases: a) $k^2 \prec D \cdot m$: Case of oscillation

b) $k^2 = 4 \cdot D \cdot m$ aperiodic limiting case

c) $k^2 > 4 \cdot D \cdot m$ crawl speed

w imaginary :

System returns exponentielly to rest position, as b)



4.2. Forced oscillations

Force from outside F

act on periodically on an oscillatory system. mathematical treatment : $m \cdot z + k \cdot z + D \cdot z = F_0 \cdot e^{i\omega t}$

Ansatz for z:
$$z = A \cdot e^{i(\omega t - \alpha)}$$

 α : Phase shift to outside force

Derivatives:

Solution via $\begin{array}{ll} \stackrel{\cdot}{z=} i \cdot \omega \cdot e^{i(\omega t - \alpha)} \\ \stackrel{\cdot}{z=} -\omega^2 \cdot A \cdot e^{i(\omega t - \alpha)} \Rightarrow \end{array}$ differential equation $-\omega^2 \cdot m \cdot A \cdot e^{i(\omega t - \alpha)} + i \cdot k \cdot \omega \cdot A \cdot e^{i(\omega t - \alpha)}$ $+D \cdot A \cdot e^{i(\omega t - \alpha)} = F_0 \cdot e^{i\omega t}$ $-\omega^2 \cdot m \cdot A + i \cdot k \cdot \omega \cdot A + D \cdot A = \frac{F_0 \cdot e^{i\alpha}}{4}$ $m(\frac{D}{m} - \omega^2) + ik \cdot \omega = \frac{F_0 \cdot e^{i\alpha}}{4} \implies m(\omega_0^2 - \omega^2) + ik \cdot \omega = \frac{F_0}{4}(\cos \alpha + i \sin \alpha)$

$$m(\omega_0^2 - \omega^2) + ik \cdot \omega = \frac{F_0}{A}(\cos \alpha + i \sin \alpha)$$

